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> DÉPARTEMENT D2 – FLUIDES THERMIQUE ET COMBUSTION

An introduction to hydrodynamic stability

Lecture 5: Spatial and spatiotemporal stability

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- 1. A quick recap. of lecture 4
- 2. The spatial stability problem
 - Augmented eigenvalue problem
 - Using the linearised equations in full form
 - Spatial stability of mixing layer
 - Getting to know the spectrum
 - notion of basis
 - notion of projection (biorthogonal projection)
 - group and phase velocities
 - discrete and continous mode
 - Spatial stability of the mixing layer
 - Compressible round jet
- 3. The spatiotemporal stability problem
- 4. Non-parallel flows & global stability

1. Recap. of lecture 4

Orr-Sommerfeld equation incorporates effects of viscosity

$$(U-c)\left(\frac{\mathrm{d}^{2}\mathbf{v}(y)}{\mathrm{d}y^{2}}-\alpha^{2}\mathbf{v}(y)\right)-\frac{\mathrm{d}^{2}U}{\mathrm{d}y^{2}}\mathbf{v}(y)=\frac{1}{i\alpha\mathrm{Re}}\left(\frac{\mathrm{d}^{4}\mathbf{v}(y)}{\mathrm{d}y^{4}}-2\alpha^{2}\frac{\mathrm{d}^{2}\mathbf{v}(y)}{\mathrm{d}y^{2}}+\alpha^{4}\mathbf{v}(y)\right)$$
(103)

Fourth-order equation, requires 4 boundary conditions

Technique for imposing homogeneous Dirichlet BC:



The importance of testing for convergence



Critical Reynolds number and the neutral stability curve





Boundary layer instability: the subtle effect of base flow



Rayleigh's inflection-point theorem

$$\int_{a}^{b} [|\phi_{y}|^{2} + \alpha^{2}|\phi|^{2} dy + \int_{a}^{b} \frac{U_{yy}(U - c_{r})}{|U - c|^{2}} |\phi|^{2} dy = 0$$
$$c_{i} \int_{a}^{b} \frac{U_{yy}}{|U - c|^{2}} |\phi|^{2} dy = 0$$

A necessary (but non sufficient) condition for INVISCID INSTABILITY is that $U_{yy}(y_s) = 0$ -> Mean curvature (rate of change of vorticity) changes sign.

A flow without an inflection point will be INVISCIDLY STABLE

Neutral stability curves for inviscidly unstable (I) and inviscidly stable (II) shear-flow



2. The spatial stability problem



In spatially developing flows, spatial stability seems more appropriate (Gaster 1962, 1965)



Brown & Roshko JFM 1974





Figure 1 Smoke-flow visualization in the boundary layer over an axisymmetric body. Photograph by F. N. M. Brown (courtesy of the University of Notre Dame).



In spatially developing flows, spatial stability seems more appropriate (Gaster 1962, 1965)



Spatial stability

Orr-Sommerfeld equation

$$(U-c)\left(\frac{\mathrm{d}^{2}\mathbf{v}(y)}{\mathrm{d}y^{2}}-\alpha^{2}\mathbf{v}(y)\right)-\frac{\mathrm{d}^{2}U}{\mathrm{d}y^{2}}\mathbf{v}(y)=\frac{1}{i\alpha\mathrm{Re}}\left(\frac{\mathrm{d}^{4}\mathbf{v}(y)}{\mathrm{d}y^{4}}-2\alpha^{2}\frac{\mathrm{d}^{2}\mathbf{v}(y)}{\mathrm{d}y^{2}}+\alpha^{4}\mathbf{v}(y)\right)$$
(103)

Fourth-order, 4 boundary conditions

Rayleigh equation

$$(U-c)\left(\frac{\mathrm{d}^2\mathbf{v}(y)}{\mathrm{d}y^2} - \alpha^2\mathbf{v}(y)\right) - \frac{\mathrm{d}^2U}{\mathrm{d}y^2}\mathbf{v}(y) = 0$$

Second-order, 2 boundary conditions

Derivation didn't specify temporal or spatial stability

Now, $\omega(=\alpha c)$, is a real-valued parameter, α , is a complex-valued eigenvalue

Spatial stability

Orr-Sommerfeld equation

$$(U-c)\left(\frac{\mathrm{d}^2\mathbf{v}(y)}{\mathrm{d}y^2} - \alpha^2\mathbf{v}(y)\right) - \frac{\mathrm{d}^2U}{\mathrm{d}y^2}\mathbf{v}(y) = \frac{1}{i\alpha\mathrm{Re}}\left(\frac{\mathrm{d}^4\mathbf{v}(y)}{\mathrm{d}y^4} - 2\alpha^2\frac{\mathrm{d}^2\mathbf{v}(y)}{\mathrm{d}y^2} + \alpha^4\mathbf{v}(y)\right)$$
(103)

Fourth-order, 4 boundary conditions

Multiply by $\alpha\,$ to obtain

$$\left[(\alpha U - \omega) \left(\frac{\mathrm{d}^2}{\mathrm{d}y^2} - \alpha^2 \right) - \alpha U'' + \frac{i}{R} \left(\frac{\mathrm{d}^2}{\mathrm{d}y^2} - \alpha^2 \right) \right] \hat{v} = 0$$

Eigenvalue now appears non-linearly.

Spatial stability

$$\left[(\alpha U - \omega) \left(\frac{\mathrm{d}^2}{\mathrm{d}y^2} - \alpha^2 \right) - \alpha U'' + \frac{i}{R} \left(\frac{\mathrm{d}^2}{\mathrm{d}y^2} - \alpha^2 \right) \right] \hat{v} = 0$$

Eigenvalue now appears non-linearly.

Deal with this issue by constructing augmented eigenvalue problem

$$\begin{bmatrix} 0 & \mathcal{I} & 0 & 0 \\ 0 & 0 & \mathcal{I} & 0 \\ 0 & 0 & 0 & \mathcal{I} \\ -\mathcal{F}_0 & -\mathcal{F}_1 & -\mathcal{F}_2 & -\mathcal{F}_3 \end{bmatrix} \begin{bmatrix} v \\ \alpha v \\ \alpha^2 v \\ \alpha^3 v \end{bmatrix} = \alpha \begin{bmatrix} \mathcal{I} & 0 & 0 & 0 \\ 0 & \mathcal{I} & 0 & 0 \\ 0 & 0 & \mathcal{I} & 0 \\ 0 & 0 & 0 & \mathcal{F}_4 \end{bmatrix} \begin{bmatrix} v \\ \alpha v \\ \alpha^2 v \\ \alpha^3 v \end{bmatrix}$$

Exercises: 1. Obtain $-\mathcal{F}_0$ $-\mathcal{F}_1$ $-\mathcal{F}_2$ $-\mathcal{F}_3$ \mathcal{F}_4

2. Spatial stability of tanh profile

2. The spatial stability problem

$$\begin{bmatrix} 0 & \mathcal{I} & 0 & 0 \\ 0 & 0 & \mathcal{I} & 0 \\ 0 & 0 & 0 & \mathcal{I} \\ -\mathcal{F}_0 & -\mathcal{F}_1 & -\mathcal{F}_2 & -\mathcal{F}_3 \end{bmatrix} \begin{bmatrix} v \\ \alpha v \\ \alpha^2 v \\ \alpha^3 v \end{bmatrix} = \alpha \begin{bmatrix} \mathcal{I} & 0 & 0 & 0 \\ 0 & \mathcal{I} & 0 & 0 \\ 0 & 0 & \mathcal{I} & 0 \\ 0 & 0 & 0 & \mathcal{F}_4 \end{bmatrix} \begin{bmatrix} v \\ \alpha v \\ \alpha^2 v \\ \alpha^3 v \end{bmatrix}$$

$$\begin{aligned} \mathcal{F}_{0,O} &= -\mathrm{i}\omega\mathcal{D}^2 - \frac{1}{R}\mathcal{D}^4 & \mathcal{F}_{3,O} &= -\mathrm{i}U\mathcal{I} \\ \mathcal{F}_{1,O} &= \mathrm{i}U\mathcal{D}^2 - \mathrm{i}U''\mathcal{I} & \mathcal{F}_{4,O} &= -\frac{1}{R}\mathcal{I}, \\ \mathcal{F}_{2,O} &= \mathrm{i}\omega\mathcal{I} + \frac{2}{R}\mathcal{D}^2 & \mathcal{F}_{4,O} &= -\frac{1}{R}\mathcal{I}, \end{aligned}$$

Spatial stability using the complete set of linearised equations

$$u_t + Uu_x + U'v = -p_x + \Delta u/Re,$$

$$v_t + Uv_x = -p_y + \Delta v/Re,$$

$$u_x + v_y = 0$$

In matrix form

$$0 = \begin{bmatrix} -\begin{pmatrix} \partial_t & 0 & 0 \\ 0 & \partial_t & 0 \\ 0 & 0 & 0 \end{pmatrix} + \begin{pmatrix} -U\partial_x + \Delta/Re & U' & -\partial_x \\ 0 & -U\partial_x + \Delta/Re & -\partial_y \\ \partial_x & \partial_y & 0 \end{pmatrix} \end{bmatrix} \begin{pmatrix} u \\ v \\ p \end{pmatrix}$$

Introduce normal modes

$$u = \hat{u}(y) \mathrm{e}^{ikx - i\omega t}$$

$$0 = \begin{bmatrix} -\begin{pmatrix} \partial_t & 0 & 0 \\ 0 & \partial_t & 0 \\ 0 & 0 & 0 \end{pmatrix} + \begin{pmatrix} -U\partial_x + \Delta/Re & U' & -\partial_x \\ 0 & -U\partial_x + \Delta/Re & -\partial_y \\ \partial_x & \partial_y & 0 \end{pmatrix} \end{bmatrix} \begin{pmatrix} u \\ v \\ p \end{pmatrix}$$

Becomes, after Fourier transform from x - t to $\omega - k$, i.e. $\partial_t \to -i\omega$, $\partial_x \to ik$, $\partial_{xx} \to -k^2$.

$$0 = \left[-\omega \underbrace{\begin{pmatrix} -i & 0 & 0 \\ 0 & -i & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{E} + \underbrace{\begin{pmatrix} \partial_{yy}/Re & U' & 0 \\ 0 & \partial_{yy}/Re & -D \\ 0 & D & 0 \end{pmatrix}}_{A_{00}} + k \underbrace{\begin{pmatrix} -iU & 0 & -i \\ 0 & -iU & 0 \\ i & 0 & 0 \end{pmatrix}}_{A_{1}} + k^{2} \underbrace{\begin{pmatrix} -I/Re & 0 & 0 \\ 0 & -I/Re & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{A_{2}} \right] \underbrace{\begin{pmatrix} \hat{u} \\ \hat{v} \\ \hat{p} \end{pmatrix}}_{\hat{q}}$$

2. The spatial stability problem

$$0 = \begin{bmatrix} -\omega \underbrace{\begin{pmatrix} -i & 0 & 0 \\ 0 & -i & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{E} + \underbrace{\begin{pmatrix} \partial_{yy}/Re & U' & 0 \\ 0 & \partial_{yy}/Re & -D \\ 0 & D & 0 \end{pmatrix}}_{A_{00}} + k \underbrace{\begin{pmatrix} -iU & 0 & -i \\ 0 & -iU & 0 \\ i & 0 & 0 \end{pmatrix}}_{A_{1}} + k^{2} \underbrace{\begin{pmatrix} -I/Re & 0 & 0 \\ 0 & -I/Re & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{A_{2}} \end{bmatrix} \underbrace{\begin{pmatrix} \hat{u} \\ \hat{v} \\ \hat{p} \end{pmatrix}}_{\hat{q}}$$

Temporal eigenvalue problem $\omega E\hat{q} = A\hat{q}$

Spatial eigenvalue problem

 $0 = (A_0 + kA_1 + k^2 A_2)\hat{q}_1$

with $A_0 = -\omega E + A_{00}$

Can be solved in Matlab with k=polyeig(A0,A1,A2)

Or, alternatively, by building an augmented system, as we did with the Orr-Sommerfeld equation, and then solving using eig



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2. The spatial stability problem

The continuous spectrum

$$\frac{\partial^2 u}{\partial t^2} = \frac{\partial^2 u}{\partial x^2}$$
$$\frac{\mathrm{d}f}{\mathrm{d}x^2} + \omega^2 f = 0$$

Bounded domain u(0,t) = u(1,t) = 0

Solution:
$$\omega_n = n\pi$$
, $f_n(x) = 2^{-1/2} \sin n\pi x$, $n = 1, 2, 3...$

Infinite number of discrete eigenvalues and eigenfunctions (harmonics of guitar string)

Unbounded domain u(0,t) = u(x,t) bounded as $x \to \infty$

Solution:
$$\omega$$
 real and $\omega \ge 0$ $f(x; \omega) = (2\pi)^{-1/2} \sin \omega x$

A continuum of eigenvalues and eigenfunctions: semi-infinite guitar string, harmonics approach one another and become a continuum.

Eigenspectra of unbounded flows



FIGURE 3.4. Spectrum for Blasius boundary layer flow for $\alpha = 0.2$, Re = 500 (a) Numerically obtained spectrum displaying a discrete representation of the continuous spectrum with a particular choice of discretization parameters (b) Exact spectrum displaying the discrete and continuous part.

Compressible round jet



Governing equations

$$\begin{split} \overline{\rho} \Big(\frac{Du_x}{Dt} + \frac{\partial \overline{U}_x}{\partial r} u_r + \frac{1}{r} \frac{\partial \overline{U}_x}{\partial \theta} u_\theta \Big) &= -\frac{\partial p}{\partial x} + \frac{1}{\operatorname{Re}} V_x, \\ \overline{\rho} \frac{Du_r}{Dt} &= -\frac{\partial p}{\partial r} + \frac{1}{\operatorname{Re}} V_r, \\ \overline{\rho} \frac{Du_\theta}{Dt} &= -\frac{1}{r} \frac{\partial p}{\partial \theta} + \frac{1}{\operatorname{Re}} V_\theta, \\ \overline{\rho} \Big(\frac{DT}{Dt} + (\gamma - 1) \overline{T} \nabla \cdot \mathbf{u} \Big) &= \frac{\gamma}{\operatorname{Re}} \phi + \frac{\gamma}{\operatorname{Re}\operatorname{Pr}} \nabla \cdot \mathbf{Q}, \\ \frac{D\rho}{Dt} + \overline{\rho} \nabla \cdot \mathbf{u} &= 0, \\ p &= \frac{\gamma - 1}{\gamma} (\overline{T} \rho + \overline{\rho} T). \end{split}$$

Compressible round jet



Governing equations in matrix form

$$\frac{\partial \mathbf{q}}{\partial t} + \mathbf{A}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial r} + \mathbf{B}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial x} + \mathbf{C}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial \theta} + \mathbf{D}(\overline{\mathbf{Q}})\mathbf{q} = 0,$$

$$\overline{\mathbf{Q}} = (\overline{U}_x(r), 0, 0, \overline{\rho}, \overline{T})$$

$$\mathbf{q}(r) = (u_x(r), u_r(r), u_\theta(r), \rho(r), T(r))$$

Compressible round jet



Governing equations in matrix form

$$\frac{\partial \mathbf{q}}{\partial t} + \mathbf{A}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial r} + \mathbf{B}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial x} + \mathbf{C}(\overline{\mathbf{Q}})\frac{\partial \mathbf{q}}{\partial \theta} + \mathbf{D}(\overline{\mathbf{Q}})\mathbf{q} = 0,$$

Introduce normal modes, $q(x, r, \theta, t) = \hat{\mathbf{q}}(r) e^{i\alpha(x-ct)} e^{im\theta}$

To give eigenvalue problem,

$$\mathbf{A}\frac{\mathrm{d}\hat{\mathbf{q}}}{\mathrm{d}r} + (-i\omega\mathbf{I} + i\alpha\mathbf{B} + im\mathbf{C} + \mathbf{D})\hat{\mathbf{q}} = 0.$$



Group versus phase velocity

Phase velocity

Temporal stability

$$U_c = \operatorname{Re}(c) = \frac{\operatorname{Re}(\omega)}{\alpha}$$

Spatial stability

$$U_c = \frac{\omega}{\operatorname{Re}(\alpha)}$$

Velocity at which phase fronts move

Group versus phase velocity

Group velocity $U_g = \frac{\partial \omega}{\partial \alpha}$ Ug U,

Velocity at which energy travels

2. The spatial stability problem



Group versus phase velocity

Group velocity



FIGURE 13-6 When two wave functions having frequencies very close together are summed, the phenomenon of beats (slowly varying amplitude) is observed.

Identifying sign of group velocity



Identifying sign of group velocity


Identifying sign of group velocity



Compressible, viscous round jet



Example of modes with opposite phase and group velocity



Brès, Jordan, Jaunet, Cavalieri, Towne, Lele, Colonius, Schmidt, JFM 2018



Towne, Cavalieri, Jordan, Colonius, Schmidt, Jaunet & Brès, JFM 2017.

Presentation based on chapter 4 of « Perspectives in Fluid Dynamics » (2000): « Open shear-flow instabilities » by P. Huerre. In temporal and spatial stability problems we impose real wavenumber or frequency, i.e. we assume something about the system.

A more general approach would involve not making any such assumption.

In which case we can learn about the stability behaviour of the system by computing its impulse response, i.e. its Green's function.

All of the salient behaviour can be understood by considering a simplified system, with no cross-stream (y) direction, because this direction is described by eigenfunctions that are slaved to the eigenvalues.

We will therefore consider the impulse response of an equation of this form:

$$\mathcal{D}\Big[-i\frac{\partial}{\partial x}, i\frac{\partial}{\partial t}; R\Big]G(x,t) = \delta(x)\delta(t)$$

The Ginzburg-Landau equation is frequently used for this,

$$\left(\frac{\partial}{\partial t} + U\frac{\partial}{\partial x}\right)\psi - \mu\psi - (1 + ic_d)\frac{\partial^2\psi}{\partial x^2} = 0$$

Impulse response, solution of,

$$\mathcal{D}\Big[-i\frac{\partial}{\partial x}, i\frac{\partial}{\partial t}; R\Big]G(x,t) = \delta(x)\delta(t)$$

provides a complete characterisation of the stability behaviour of the system.



Complex frequency-wavenumber analysis of,

$$\mathcal{D}\Big[-i\frac{\partial}{\partial x}, i\frac{\partial}{\partial t}; R\Big]G(x,t) = \delta(x)\delta(t)$$

allows connection with wavenumber-frequency space we've been working in up to now. We consider the Fourier-transformed system,

$$\mathcal{D}(k,\omega)G(k,\omega) = 1$$
$$G(k,\omega) = \frac{1}{\mathcal{D}(k,\omega)}$$



In space-time the impulse response will be retrieved by,

$$G(x,t) = \int_{L_{\omega}} \int_{F_k} G(k,\omega) \mathrm{e}^{i(kx-\omega t)} \mathrm{d}k \mathrm{d}\omega$$

$$G(x,t) = \int_{L_{\omega}} \int_{F_{k}} G(k,\omega) e^{i(kx-\omega t)} dkd\omega$$

$$G(x,t) = \int_{L_{\omega}} \int_{F_{k}} \frac{1}{\mathcal{D}(k,\omega)} e^{i(kx-\omega t)} dkd\omega$$

Much of the subtlety involved in computing and understanding the impulse response has to do with the integration paths L_ω & F_k

To see this, first consider the frequency/time transform

$$G(k,t) = \int_{L_{\omega}} \frac{1}{\mathcal{D}(k,\omega)} e^{-i\omega t} d\omega$$

 $\alpha_{\rm r}$

$$G(k,t) = \int_{L_{\omega}} \frac{1}{\mathcal{D}(k,\omega)} e^{-i\omega t} d\omega$$

Technique for solving integral: closed integration contours containing the pole singularities: two semicircles closed at infinity. Residue Theorem then provides solution.

Contribution from integration along the semicircular paths must be zero.

The integrand must therefore decay exponentially for $\omega_I
ightarrow \pm \infty$

- upper and lower half planes correspond, respectively, to $\,t < 0\,$ & $\,t > 0\,$





This, and causality, dictate the position of the integration path, L_ω





This, and causality, dictate the position of the integration path, L_{ω}





Once the integration paths have been determined, standard complex-variable techniques can be used to first evaluate the integral,

$$G(k,t) = \int_{L_{\omega}} \frac{1}{\mathcal{D}(k,\omega)} e^{-i\omega t} d\omega$$

The integrand is dominated by pole singularities associated with the zeros of $\mathcal{D}(k,\omega)$ i.e. the modes $\omega_i(k)$



We now need to perform the inverse wavenumber transform

$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} \frac{\mathrm{e}^{-i\omega(k)t}}{\frac{\partial \mathcal{D}}{\partial \omega} [k,\omega(k)]} \mathrm{e}^{ikx} \mathrm{d}k$$
$$= -\frac{i}{2\pi} \int_{F_k} \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega} [k,\omega(k)]} \mathrm{e}^{i(kx-\omega(k)t)} \mathrm{d}k$$

This expression falls into the general class of integrals of the form

$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

with

$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k, \omega(k)]} \qquad \qquad \rho\left(k; \frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$

$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) e^{\rho(k;x/t)t} dk \qquad \qquad \rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

As we're interested in the long-time response, t is a large parameter, and





$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) e^{\rho(k;x/t)t} dk \qquad \qquad \rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

As we're interested in the long-time response, *t* is a large parameter.

A characteristic of this kind of integral is the presence, in the integrand, of a fast exponential associated with the large parameter, *t*,

https://en.wikipedia.org/wiki/Method_of_steepest_descent

The method of Steepest Descent is suited to obtain asymptotic approximations as

$$t \to \infty$$
 along $\frac{x}{t} = \text{const.}$



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

https://en.wikipedia.org/wiki/Method_of_steepest_descent

For large time, the order of magnitude of the integrand is controlled, at leading order, by the real part of the exponent, i.e. by the height of $\rho_R(k;x/t)$



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

For large time, the order of magnitude of the integrand is controlled, at leading order, by the real part of the exponent, i.e. by the height of $\rho_R(k;x/t)$



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

The complex function, $\
ho(k;x/t)\,$, has a stationary (saddle) point, k_o

$$\frac{\partial \rho}{\partial k} \left(k_o; \frac{x}{t} \right) = i \left[\frac{x}{t} - \frac{\partial \omega}{\partial k} (k_o) \right] = 0$$

The dominant contribution comes from the neighbourhood of,

$$\rho\left(k_o;\frac{x}{t}\right)$$



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

Next step: deform the integration path, F_k , into the steepest descent path, F_p .



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

Next step: deform the integration path, F_k , into the steepest descent path, $F_p\,$.

The dominant contribution comes from the neighbourhood of,

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$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
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Next step: deform the integration path, F_k , into the steepest descent path, F_p .

The dominant contribution comes from the neighbourhood of,

$$\rho\left(k_o; \frac{x}{t}\right)$$

 To leading order integral restricted to small segment around k_o



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

Next step: deform the integration path, F_k , into the steepest descent path, F_p .

Steepest descent approach:

$$\rho\left(k;\frac{x}{t}\right) \approx \rho\left(k_o;\frac{x}{t}\right) + \frac{1}{2}\frac{\partial^2\rho}{\partial k^2}\left(k_o;\frac{x}{t}\right)(k-k_o)^2$$

along path of steepest descent.



$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

All of that math leads to solution,

$$G(x,t) \approx \frac{f(k_o)}{\sqrt{2\pi \frac{\partial^2 \rho}{\partial k^2} \left(k_o; \frac{x}{t}\right)}} e^{\rho(k_o; x/t)t}$$
$$\approx \frac{e^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

The asymptotic solution is entirely determined, to leading order, by what's happening at the saddle point.

$$G(x,t) = -\frac{i}{2\pi} \int_{F_k} f(k) \mathrm{e}^{\rho(k;x/t)t} \mathrm{d}k$$

$$\rho\left(k;\frac{x}{t}\right) = i\left[k\frac{x}{t} - \omega(k)\right]$$
$$f(k) = \frac{1}{\frac{\partial \mathcal{D}}{\partial \omega}[k,\omega(k)]}$$

The impulse response, along each ray,
$$\frac{x}{t} = \text{const.}$$
, is:

$$G(x,t) \approx \frac{e^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega}[k_o, \omega(k_o)]\sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2}(k_o)t}}$$

where the complex wavenumber, k_o , is given by the saddle-point condition,

$$\frac{\partial \rho}{\partial k} \left(k_o; \frac{x}{t} \right) = i \left[\frac{x}{t} - \frac{\partial \omega}{\partial k} (k_o) \right] = 0 \quad \longrightarrow$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

Group velocity associated with the saddle point

$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$



Group velocity associated with the saddle point

Physical interpretation

- Asymptotic impulse response takes form of wavepacket

- Observer moving on ray, V=x/t , perceives, complex frequency, $\omega_o=\omega(k_o)$, and complex wavenumber, k_o



$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

Physical interpretation

- Observer moving on ray, $V=x/t\,$, perceives a temporal growth,

$$\mathbf{e}^{\sigma t} = \mathbf{e}^{\left(\omega_{oI} - \frac{x}{t}k_{oI}\right)t}$$



$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

$$\mathbf{e}^{\sigma t} = \mathbf{e}^{\left(\omega_{oI} - \frac{x}{t}k_{oI}\right)t}$$

Physical interpretation

Domain occupied by instability

$$\sigma\Big(\frac{x}{t}\Big) > 0$$



$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

$$\mathbf{e}^{\sigma t} = \mathbf{e}^{\left(\omega_{oI} - \frac{x}{t}k_{oI}\right)t}$$

Physical interpretation

Two important modes:

1. Maximum mode, (ω_{max}, k_{max}) , travelling at which has highest overall growth rate

 $\frac{\partial \omega}{\partial k}\Big|_{\omega_{abs}}$

= 0

2. Absolute mode, travelling at which provides growth rate in laboratory reference frame

$$\left. \frac{\partial \omega}{\partial k} \right|_{\omega_{max}} = V_{max}$$



The maximum mode of the impulse response is identical to the temporal mode with highest growth rate

$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

$$\mathbf{e}^{\sigma t} = \mathbf{e}^{\left(\omega_{oI} - \frac{x}{t}k_{oI}\right)t}$$

Absolute mode
$$(\omega_{abs},k_{abs})$$
 ;

$$\left. \frac{\partial \omega}{\partial k} \right|_{k_{abs}} = 0 \quad ; \quad \omega_{abs,I}$$



$$G(x,t) \approx \frac{\mathrm{e}^{i[\pi/4 + k_o x - \omega(k_o)t]}}{\frac{\partial \mathcal{D}}{\partial \omega} [k_o, \omega(k_o)] \sqrt{2\pi \frac{\partial^2 \omega}{\partial k^2} (k_o)t}}$$

$$\frac{\partial \omega}{\partial k}(k_o) = \frac{x}{t}$$

$$\mathbf{e}^{\sigma t} = \mathbf{e}^{\left(\omega_{oI} - \frac{x}{t}k_{oI}\right)t}$$

Physical interpretation

Résumé





Stability criteria:

$$\begin{split} & \omega_{max,I} < 0 & \longrightarrow & \text{temporal growth negative} \\ & \text{for all } V = x/t \\ & \text{flow linearly stable.} \end{split} \\ & \omega_{max,I} > 0 & \longrightarrow & \text{temporal growth positive in} \\ & \text{finite range of } V = x/t \\ & \text{flow linearly unstable.} \end{aligned} \\ & \omega_{abs,I} < 0 & \longrightarrow & \text{temporal growth rate negative} \\ & \omega_{abs,I} > 0 & \longrightarrow & \text{temporal growth rate negative} \\ & \omega_{abs,I} > 0 & \longrightarrow & \text{temporal growth rate positive} \\ & \omega_{abs,I} > 0 & \longrightarrow & \text{temporal growth rate positive} \\ & \text{in lab. reference frame,} \\ & \text{absolutely stable.} \end{split}$$

absolutely unstable.

Isothermal jet: convectively unstable





Heated jet: absolutely unstable





Mixing layer: convectively unstable

Cylinder wake: absolutely unstable

Amplifier flow



Without continual forcing flow will re laminarise

Oscillator flow



R = 161

Instability is self-sustained, does not require forcing




4. From non-parallel flow to global modes

Recall step 3 in derivation of local stability problems: Identification of BASE-FLOW

- Parallel and 2D (if flow changes slowly in some direction a locally parallel approximation is often adequate)



A necessary step for derivation of Orr-Sommerfeld equation (an ODE).

Recall step 3 in derivation of local stability problems: Identification of BASE-FLOW

- Parallel and 2D (if flow changes slowly in some direction a locally parallel approximation is often adequate)



Strictly only true for some wall-bounded flows (Poiseuille, Couette), Shear flows are generally non-parallel due to momentum diffusion by viscosity.

4. Non-parallel flows

Parallel versus non-parallel flows



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Slowly diverging flows

Definition: U(x, y) $x \text{ is 'slow' variable} \longrightarrow \frac{dU}{dx} = \epsilon \frac{dU}{dy}$

$$v(x, y, z, t) = \hat{v}(y) e^{i(\alpha x + \beta z - \omega t)}$$

Method of multiple scales (Bouthier '72, Gaster '74, Crighton & Gaster '76) show that solution takes form

Slowly diverging flows

Method of multiple scales (Bouthier '72, Gaster '74, Crighton & Gaster '76) show that solution takes form

 $\hat{v}(x,y) \ \& \ lpha(x)$ can be found by expanding linearised Navier-Stokes equations in powers of $\,\epsilon$

Equations at successive order remain ODE.

The mathematics is complicated...

Parabolised stability equations

$$v(x, y, z, t) = \hat{v}(x, y) e^{i \int_0^x \alpha(x') dx'} e^{i(\beta z - \omega t)}$$

- We know that the solution for slowly diverging flow has this shape
- Substitute directly into the linearised Navier-Stokes equations
- This gives the Parabolised Stability Equations (Herbert 1997)

Parabolised stability equations - results for Blasius boundary layer



Figure 2 The neutral curves of the LST and for nonparallel flow according to PSE and Gaster (1974). (Data of Bertolotti et al 1992.)

Parabolised stability equations



As α_I changes sign, amplification switches to decay



Computation considerations

1D
$$v(x, y, z, t) = \hat{v}(y) e^{i(\alpha x + \beta z - \omega t)}$$

 N_y degrees of freedom

2D
$$v(x, y, z, t) = \hat{v}(x, y) e^{i(\beta z - \omega t)}$$

 $N_x \times N_y$ degrees of freedom

3D
$$v(x, y, z, t) = \hat{v}(x, y, z) e^{-i\omega t}$$

 $N_x \times N_y \times N_z$ degrees of freedom

- Simplify whenever possible
- Stability of non-parallel flows is currently feasible
- Direct solution of eigenvalue problem usually avoided. Iterative, Arnoldi method preferred: focus on limited number of modes.

Typical matrix size

Theofilis 2003

~ 1 Mbytes

~ 4.3 Gbytes

~ 17.6 Tbytes

2D example: cylinder wake (Noack & Eckelmann 1994)



Global stability analysis of the cylinder wake

3D example: jet in cross flow (Bagheri et al. 2009)



FIGURE 5. The most unstable mode $((\lambda_r, \lambda_i) = (0.068, 1.06))$ seen from two different angles, marked with S_1 in figure 4, is shown with red λ_2 isocontours. The base flow is shown in blue (λ_2) and grey (u).

2.5D example: turbulent jet

Schmidt, Towne, Colonius, Cavalieri, Jordan, Brès, JFM 2017.

